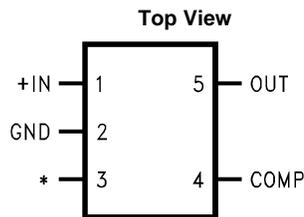


Figure 2. LM3420 Functional Diagram

Connection Diagrams

5-Lead Small Outline Package



*No internal connection, but should be soldered to PC board for best heat transfer.

Figure 3. SOT-23 Package
See Package DBV0005A

Actual Size



Figure 4. SOT-23 Package
See Package DBV0005A



These devices have limited built-in ESD protection. The leads should be shorted together or the device placed in conductive foam during storage or handling to prevent electrostatic damage to the MOS gates.

ABSOLUTE MAXIMUM RATINGS⁽¹⁾⁽²⁾

Input Voltage V(IN)		20V
Output Current		20 mA
Junction Temperature		150°C
Storage Temperature		-65°C to +150°C
Lead Temperature	Vapor Phase (60 seconds)	+215°C
	Infrared (15 seconds)	+220°C
Power Dissipation ($T_A = 25^\circ\text{C}$) ⁽³⁾		300 mW
ESD Susceptibility ⁽⁴⁾	Human Body Model	1500V

- (1) Absolute Maximum Ratings indicate limits beyond which damage to the device may occur. Operating Ratings indicate conditions for which the device is intended to be functional, but do not ensure specific performance limits. For ensured specifications and test conditions, see the Electrical Characteristics. The specified specifications apply only for the test conditions listed. Some performance characteristics may degrade when the device is not operated under the listed test conditions.
- (2) If Military/Aerospace specified devices are required, please contact the Texas Instruments Sales Office/Distributors for availability and specifications.
- (3) The maximum power dissipation must be derated at elevated temperatures and is dictated by T_{Jmax} (maximum junction temperature), θ_{JA} (junction to ambient thermal resistance), and T_A (ambient temperature). The maximum allowable power dissipation at any temperature is $P_{Dmax} = (T_{Jmax} - T_A)/\theta_{JA}$ or the number given in the Absolute Maximum Ratings, whichever is lower. The typical thermal resistance (θ_{JA}) when soldered to a printed circuit board is approximately 306°C/W for the DBV0005A package.
- (4) The human body model is a 100 pF capacitor discharged through a 1.5 kΩ resistor into each pin.

OPERATING RATINGS⁽¹⁾⁽²⁾

Ambient Temperature Range	$-40^{\circ}\text{C} \leq T_A \leq +85^{\circ}\text{C}$
Junction Temperature Range	$-40^{\circ}\text{C} \leq T_J \leq +125^{\circ}\text{C}$
Output Current	15 mA

- (1) Absolute Maximum Ratings indicate limits beyond which damage to the device may occur. Operating Ratings indicate conditions for which the device is intended to be functional, but do not ensure specific performance limits. For ensured specifications and test conditions, see the Electrical Characteristics. The specified specifications apply only for the test conditions listed. Some performance characteristics may degrade when the device is not operated under the listed test conditions.
- (2) The maximum power dissipation must be derated at elevated temperatures and is dictated by T_{Jmax} (maximum junction temperature), θ_{JA} (junction to ambient thermal resistance), and T_A (ambient temperature). The maximum allowable power dissipation at any temperature is $P_{Dmax} = (T_{Jmax} - T_A)/\theta_{JA}$ or the number given in the Absolute Maximum Ratings, whichever is lower. The typical thermal resistance (θ_{JA}) when soldered to a printed circuit board is approximately 306°C/W for the DBV0005A package.

**LM3420-4.2
ELECTRICAL CHARACTERISTICS**

Specifications with standard type face are for $T_J = 25^{\circ}\text{C}$, and those with **boldface type** apply over **full Operating Temperature Range**. Unless otherwise specified, $V(IN) = V_{REG}$, $V_{OUT} = 1.5V$.

Symbol	Parameter	Conditions	Typical ⁽¹⁾	LM3420A-4.2 Limit ⁽²⁾	LM3 420-4.2 Limit ⁽²⁾	Units (Limits)
V_{REG}	Regulation Voltage	$I_{OUT} = 1 \text{ mA}$	4.2	4.221/ 4.242 4.179/ 4.158	4.242/ 4.284 4.158/ 4.116	V V(max) V(min)
	Regulation Voltage Tolerance	$I_{OUT} = 1 \text{ mA}$		$\pm 0.5/\pm 1$	$\pm 1/\pm 2$	%(max)
I_q	Quiescent Current	$I_{OUT} = 1 \text{ mA}$	85	110/ 115	125/ 150	μA $\mu\text{A(max)}$
G_m	Transconductance $\Delta I_{OUT}/\Delta V_{REG}$	$20 \mu\text{A} \leq I_{OUT} \leq 1 \text{ mA}$ $V_{OUT} = 2V$	3.3	1.3/ 0.75	1.0/ 0.50	mA/mV mA/mV(min)
		$1 \text{ mA} \leq I_{OUT} \leq 15 \text{ mA}$ $V_{OUT} = 2V$	6.0	3.0/ 1.5	2.5/ 1.4	mA/mV mA/mV(min)
A_V	Voltage Gain $\Delta V_{OUT}/\Delta V_{REG}$	$1V \leq V_{OUT} \leq V_{REG} - 1.2V$ (-1.3) $R_L = 200\Omega$ ⁽³⁾	1000	550/ 250	450/ 200	V/V V/V(min)
		$1V \leq V_{OUT} \leq V_{REG} - 1.2V$ (-1.3) $R_L = 2 \text{ k}\Omega$	3500	1500/ 900	1000/ 700	V/V V/V(min)
V_{SAT}	Output Saturation ⁽⁴⁾	$V(IN) = V_{REG} + 100 \text{ mV}$ $I_{OUT} = 15 \text{ mA}$	1.0	1.2/ 1.3	1.2/ 1.3	V V(max)
I_L	Output Leakage Current	$V(IN) = V_{REG} - 100 \text{ mV}$ $V_{OUT} = 0V$	0.1	0.5/ 1.0	0.5/ 1.0	μA $\mu\text{A(max)}$
R_f	Internal Feedback Resistor ⁽⁵⁾		75	94	94	k Ω k $\Omega(max)$
				56	56	k $\Omega(min)$
E_n	Output Noise Voltage	$I_{OUT} = 1 \text{ mA}$, $10 \text{ Hz} \leq f \leq 10 \text{ kHz}$	70			μV_{RMS}

- (1) Typical numbers are at 25°C and represent the most likely parametric norm.
- (2) Limits are 100% production tested at 25°C. Limits over the operating temperature range are specified through correlation using Statistical Quality Control (SQC) methods. The limits are used to calculate Averaging Outgoing Quality Level (AOQL).
- (3) Actual test is done using equivalent current sink instead of a resistor load.
- (4) $V_{SAT} = V(IN) - V_{OUT}$, when the voltage at the IN pin is forced 100 mV above the nominal regulating voltage (V_{REG}).
- (5) See [Applications](#) and [Typical Performance Characteristics](#) sections for information on this resistor.

LM3420-8.2 ELECTRICAL CHARACTERISTICS

Specifications with standard type face are for $T_J = 25^\circ\text{C}$, and those with **boldface type** apply over **full Operating Temperature Range**. Unless otherwise specified, $V(\text{IN}) = V_{\text{REG}}$, $V_{\text{OUT}} = 1.5\text{V}$.

Symbol	Parameter	Conditions	Typical ⁽¹⁾	LM3420A-8.2 Limit ⁽²⁾	LM3420-8.2 Limit ⁽²⁾	Units (Limits)
V_{REG}	Regulation Voltage	$I_{\text{OUT}} = 1\text{ mA}$	8.2	8.241/ 8.282 8.159/ 8.118	8.282/ 8.364 8.118/ 8.036	V V(max) V(min)
	Regulation Voltage Tolerance	$I_{\text{OUT}} = 1\text{ mA}$		$\pm 0.5/\pm 1$	$\pm 1/\pm 2$	%(max)
I_{q}	Quiescent Current	$I_{\text{OUT}} = 1\text{ mA}$	85	110/ 115	125/ 150	μA $\mu\text{A}(\text{max})$
G_{m}	Transconductance $\Delta I_{\text{OUT}}/\Delta V_{\text{REG}}$	$20\ \mu\text{A} \leq I_{\text{OUT}} \leq 1\text{ mA}$ $V_{\text{OUT}} = 6\text{V}$	3.3	1.3/ 0.75	1.0/ 0.50	mA/mV $\text{mA}/\text{mV}(\text{min})$
		$1\text{ mA} \leq I_{\text{OUT}} \leq 15\text{ mA}$ $V_{\text{OUT}} = 6\text{V}$	6.0	3.0/ 1.5	2.5/ 1.4	mA/mV $\text{mA}/\text{mV}(\text{min})$
A_{V}	Voltage Gain $\Delta V_{\text{OUT}}/\Delta V_{\text{REG}}$	$1\text{V} \leq V_{\text{OUT}} \leq V_{\text{REG}} - 1.2\text{V}$ (-1.3) $R_{\text{L}} = 470\ \Omega$ ⁽³⁾	1000	550/ 250	450/ 200	V/V V/V(min)
		$1\text{V} \leq V_{\text{OUT}} \leq V_{\text{REG}} - 1.2\text{V}$ (-1.3) $R_{\text{L}} = 5\text{ k}\Omega$	3500	1500/ 900	1000/ 700	V/V V/V(min)
V_{SAT}	Output Saturation ⁽⁴⁾	$V(\text{IN}) = V_{\text{REG}} + 100\text{ mV}$ $I_{\text{OUT}} = 15\text{ mA}$	1.0	1.2/ 1.3	1.2/ 1.3	V V(max)
I_{L}	Output Leakage Current	$V(\text{IN}) = V_{\text{REG}} - 100\text{ mV}$ $V_{\text{OUT}} = 0\text{V}$	0.1	0.5/ 1.0	0.5/ 1.0	μA $\mu\text{A}(\text{max})$
R_{f}	Internal Feedback Resistor ⁽⁵⁾		176	220	220	$\text{k}\Omega$ $\text{k}\Omega(\text{max})$
				132	132	$\text{k}\Omega(\text{min})$
E_{n}	Output Noise Voltage	$I_{\text{OUT}} = 1\text{ mA}$, $10\text{ Hz} \leq f \leq 10\text{ kHz}$	140			μV_{RMS}

(1) Typical numbers are at 25°C and represent the most likely parametric norm.

(2) Limits are 100% production tested at 25°C . Limits over the operating temperature range are specified through correlation using Statistical Quality Control (SQC) methods. The limits are used to calculate Averaging Outgoing Quality Level (AOQL).

(3) Actual test is done using equivalent current sink instead of a resistor load.

(4) $V_{\text{SAT}} = V(\text{IN}) - V_{\text{OUT}}$, when the voltage at the IN pin is forced 100 mV above the nominal regulating voltage (V_{REG}).

(5) See [Applications](#) and [Typical Performance Characteristics](#) sections for information on this resistor.

LM3420-8.4 ELECTRICAL CHARACTERISTICS

Specifications with standard type face are for $T_J = 25^\circ\text{C}$, and those with **boldface type** apply over **full Operating Temperature Range**. Unless otherwise specified, $V(\text{IN}) = V_{\text{REG}}$, $V_{\text{OUT}} = 1.5\text{V}$.

Symbol	Parameter	Conditions	Typical ⁽¹⁾	LM3420A-8.4 Limit ⁽²⁾	LM3420-8.4 Limit ⁽²⁾	Units (Limits)
V_{REG}	Regulation Voltage	$I_{\text{OUT}} = 1\text{ mA}$	8.4	8.442/ 8.484 8.358/ 8.316	8.484/ 8.568 8.316/ 8.232	V V(max) V(min)
	Regulation Voltage Tolerance	$I_{\text{OUT}} = 1\text{ mA}$		$\pm 0.5/\pm 1$	$\pm 1/\pm 2$	%(max)
I_{q}	Quiescent Current	$I_{\text{OUT}} = 1\text{ mA}$	85	110/ 115	125/ 150	μA $\mu\text{A}(\text{max})$
G_{m}	Transconductance $\Delta I_{\text{OUT}}/\Delta V_{\text{REG}}$	$20\ \mu\text{A} \leq I_{\text{OUT}} \leq 1\text{ mA}$ $V_{\text{OUT}} = 6\text{V}$	3.3	1.3/ 0.75	1.0/ 0.50	mA/mV $\text{mA}/\text{mV}(\text{min})$
		$1\text{ mA} \leq I_{\text{OUT}} \leq 15\text{ mA}$ $V_{\text{OUT}} = 6\text{V}$	6.0	3.0/ 1.5	2.5/ 1.4	mA/mV $\text{mA}/\text{mV}(\text{min})$
A_{V}	Voltage Gain $\Delta V_{\text{OUT}}/\Delta V_{\text{REG}}$	$1\text{V} \leq V_{\text{OUT}} \leq V_{\text{REG}} - 1.2\text{V}$ (-1.3) $R_{\text{L}} = 470\Omega$ ⁽³⁾	1000	550/ 250	450/ 200	V/V V/V(min)
		$1\text{V} \leq V_{\text{OUT}} \leq V_{\text{REG}} - 1.2\text{V}$ (-1.3) $R_{\text{L}} = 5\text{ k}\Omega$	3500	1500/ 900	1000/ 700	V/V V/V(min)
V_{SAT}	Output Saturation ⁽⁴⁾	$V(\text{IN}) = V_{\text{REG}} + 100\text{ mV}$ $I_{\text{OUT}} = 15\text{ mA}$	1.0	1.2/ 1.3	1.2/ 1.3	V V(max)
I_{L}	Output Leakage Current	$V(\text{IN}) = V_{\text{REG}} - 100\text{ mV}$ $V_{\text{OUT}} = 0\text{V}$	0.1	0.5/ 1.0	0.5/ 1.0	μA $\mu\text{A}(\text{max})$
R_{f}	Internal Feedback Resistor ⁽⁵⁾		181	227	227	$\text{k}\Omega$ $\text{k}\Omega(\text{max})$
				135	135	$\text{k}\Omega(\text{min})$
E_{n}	Output Noise Voltage	$I_{\text{OUT}} = 1\text{ mA}$, $10\text{ Hz} \leq f \leq 10\text{ kHz}$	140			μV_{RMS}

(1) Typical numbers are at 25°C and represent the most likely parametric norm.

(2) Limits are 100% production tested at 25°C . Limits over the operating temperature range are specified through correlation using Statistical Quality Control (SQC) methods. The limits are used to calculate Averaging Outgoing Quality Level (AOQL).

(3) Actual test is done using equivalent current sink instead of a resistor load.

(4) $V_{\text{SAT}} = V(\text{IN}) - V_{\text{OUT}}$, when the voltage at the IN pin is forced 100 mV above the nominal regulating voltage (V_{REG}).

(5) See [Applications](#) and [Typical Performance Characteristics](#) sections for information on this resistor.

LM3420-12.6 ELECTRICAL CHARACTERISTICS

Specifications with standard type face are for $T_J = 25^\circ\text{C}$, and those with **boldface type** apply over **full Operating Temperature Range**. Unless otherwise specified, $V(\text{IN}) = V_{\text{REG}}$, $V_{\text{OUT}} = 1.5\text{V}$.

Symbol	Parameter	Conditions	Typical ⁽¹⁾	LM3420A-12.6 Limit ⁽²⁾	LM3420-12.6 Limit ⁽²⁾	Units (Limits)
V_{REG}	Regulation Voltage	$I_{\text{OUT}} = 1\text{ mA}$	12.6	12.663/ 12.726 12.537/ 12.474	12.726/ 12.852 12.474/ 12.348	V V(max) V(min)
	Regulation Voltage Tolerance	$I_{\text{OUT}} = 1\text{ mA}$		$\pm 0.5/\pm 1$	$\pm 1/\pm 2$	%(max)
I_{q}	Quiescent Current	$I_{\text{OUT}} = 1\text{ mA}$	85	110/ 115	125/ 150	μA $\mu\text{A}(\text{max})$
G_{m}	Transconductance $\Delta I_{\text{OUT}}/\Delta V_{\text{REG}}$	$20\ \mu\text{A} \leq I_{\text{OUT}} \leq 1\text{ mA}$ $V_{\text{OUT}} = 10\text{V}$	3.3	1.3/ 0.75	1.0/ 0.5	mA/mV mA/mV(min)
		$1\text{ mA} \leq I_{\text{OUT}} \leq 15\text{ mA}$ $V_{\text{OUT}} = 10\text{V}$	6.0	3.0/ 1.5	2.5/ 1.4	mA/mV mA/mV(min)
A_{V}	Voltage Gain $\Delta V_{\text{OUT}}/\Delta V_{\text{REG}}$	$1\text{V} \leq V_{\text{OUT}} \leq V_{\text{REG}} - 1.2\text{V}$ (-1.3) $R_{\text{L}} = 750\ \Omega$ ⁽³⁾	1000	550/ 250	450/ 200	V/V V/V(min)
		$1\text{V} \leq V_{\text{OUT}} \leq V_{\text{REG}} - 1.2\text{V}$ (-1.3) $R_{\text{L}} = 10\ \text{k}\Omega$	3500	1500/ 900	1000/ 700	V/V V/V(min)
V_{SAT}	Output Saturation ⁽⁴⁾	$V(\text{IN}) = V_{\text{REG}} + 100\text{ mV}$ $I_{\text{OUT}} = 15\text{ mA}$	1.0	1.2/ 1.3	1.2/ 1.3	V V(max)
I_{L}	Output Leakage Current	$V(\text{IN}) = V_{\text{REG}} - 100\text{ mV}$ $V_{\text{OUT}} = 0\text{V}$	0.1	0.5/ 1.0	0.5/ 1.0	μA $\mu\text{A}(\text{max})$
R_{f}	Internal Feedback Resistor ⁽⁵⁾		287	359	359	k Ω k Ω (max)
				215	215	k Ω (min)
E_{n}	Output Noise Voltage	$I_{\text{OUT}} = 1\text{ mA}$, $10\text{ Hz} \leq f \leq 10\text{ kHz}$	210			μV_{RMS}

(1) Typical numbers are at 25°C and represent the most likely parametric norm.

(2) Limits are 100% production tested at 25°C . Limits over the operating temperature range are specified through correlation using Statistical Quality Control (SQC) methods. The limits are used to calculate Averaging Outgoing Quality Level (AOQL).

(3) Actual test is done using equivalent current sink instead of a resistor load.

(4) $V_{\text{SAT}} = V(\text{IN}) - V_{\text{OUT}}$, when the voltage at the IN pin is forced 100 mV above the nominal regulating voltage (V_{REG}).

(5) See [Applications](#) and [Typical Performance Characteristics](#) sections for information on this resistor.

LM3420-16.8 ELECTRICAL CHARACTERISTICS

Specifications with standard type face are for $T_J = 25^\circ\text{C}$, and those with **boldface type** apply over **full Operating Temperature Range**. Unless otherwise specified, $V(\text{IN}) = V_{\text{REG}}$, $V_{\text{OUT}} = 1.5\text{V}$.

Symbol	Parameter	Conditions	Typical ⁽¹⁾	LM3420A-16.8 Limit ⁽²⁾	LM3420-16.8 Limit ⁽²⁾	Units (Limits)
V_{REG}	Regulation Voltage	$I_{\text{OUT}} = 1\text{ mA}$	16.8	16.884/ 16.968 16.716/ 16.632	16.968/ 17.136 16.632/ 16.464	V V(max) V(min)
	Regulation Voltage Tolerance	$I_{\text{OUT}} = 1\text{ mA}$		$\pm 0.5/\pm 1$	$\pm 1/\pm 2$	%(max)
I_{q}	Quiescent Current	$I_{\text{OUT}} = 1\text{ mA}$	85	110/ 115	125/ 150	μA $\mu\text{A}(\text{max})$
G_{m}	Transconductance $\Delta I_{\text{OUT}}/\Delta V_{\text{REG}}$	$20\ \mu\text{A} \leq I_{\text{OUT}} \leq 1\text{ mA}$ $V_{\text{OUT}} = 15\text{V}$	3.3	0.8/ 0.4	0.7/ 0.35	mA/mV mA/mV(min)
		$1\text{ mA} \leq I_{\text{OUT}} \leq 15\text{ mA}$ $V_{\text{OUT}} = 15\text{V}$	6.0	2.9/ 0.9	2.5/ 0.75	mA/mV mA/mV(min)
A_{V}	Voltage Gain $\Delta V_{\text{OUT}}/\Delta V_{\text{REG}}$	$1\text{V} \leq V_{\text{OUT}} \leq V_{\text{REG}} - 1.2\text{V}$ (-1.3) $R_{\text{L}} = 1\text{ k}\Omega$ ⁽³⁾	1000	550/ 250	450/ 200	V/V V/V(min)
		$1\text{V} \leq V_{\text{OUT}} \leq V_{\text{REG}} - 1.2\text{V}$ (-1.3) $R_{\text{L}} = 15\text{ k}\Omega$	3500	1200/ 750	1000/ 650	V/V V/V(min)
V_{SAT}	Output Saturation ⁽⁴⁾	$V(\text{IN}) = V_{\text{REG}} + 100\text{ mV}$ $I_{\text{OUT}} = 15\text{ mA}$	1.0	1.2/ 1.3	1.2/ 1.3	V V(max)
I_{L}	Output Leakage Current	$V(\text{IN}) = V_{\text{REG}} - 100\text{ mV}$ $V_{\text{OUT}} = 0\text{V}$	0.1	0.5/ 1.0	0.5/ 1.0	μA $\mu\text{A}(\text{max})$
R_{f}	Internal Feedback Resistor ⁽⁵⁾		392	490	490	k Ω k Ω (max)
				294	294	k Ω (min)
E_{n}	Output Noise Voltage	$I_{\text{OUT}} = 1\text{ mA}$, $10\text{ Hz} \leq f \leq 10\text{ kHz}$	280			μV_{RMS}

(1) Typical numbers are at 25°C and represent the most likely parametric norm.

(2) Limits are 100% production tested at 25°C . Limits over the operating temperature range are specified through correlation using Statistical Quality Control (SQC) methods. The limits are used to calculate Averaging Outgoing Quality Level (AOQL).

(3) Actual test is done using equivalent current sink instead of a resistor load.

(4) $V_{\text{SAT}} = V(\text{IN}) - V_{\text{OUT}}$, when the voltage at the IN pin is forced 100 mV above the nominal regulating voltage (V_{REG}).

(5) See [Applications](#) and [Typical Performance Characteristics](#) sections for information on this resistor.

TYPICAL PERFORMANCE CHARACTERISTICS

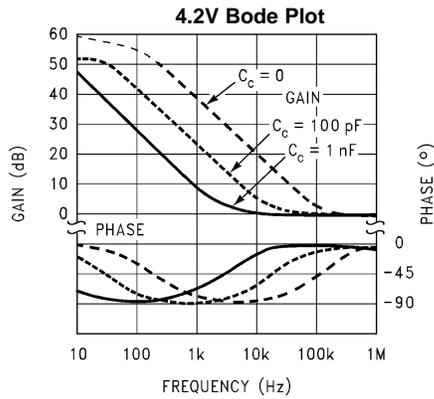


Figure 5.

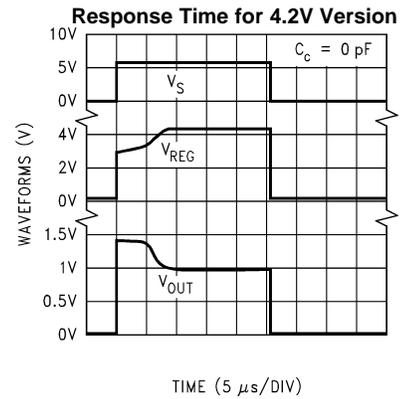


Figure 6.

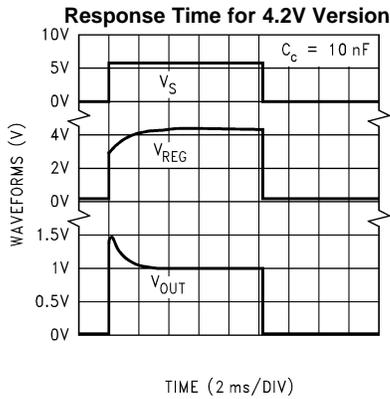


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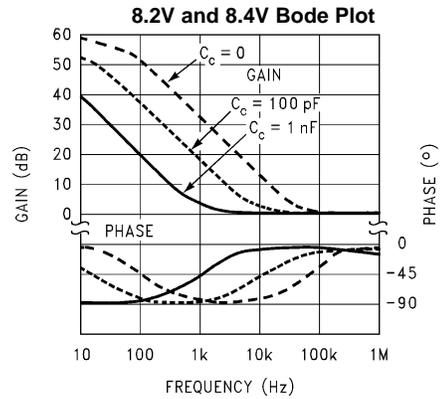


Figure 8.

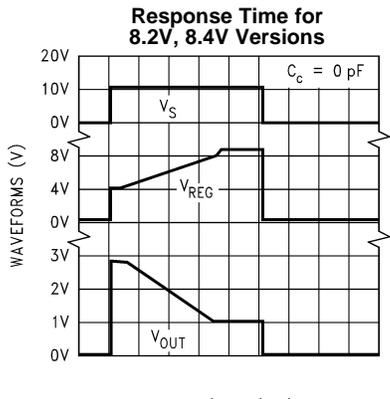


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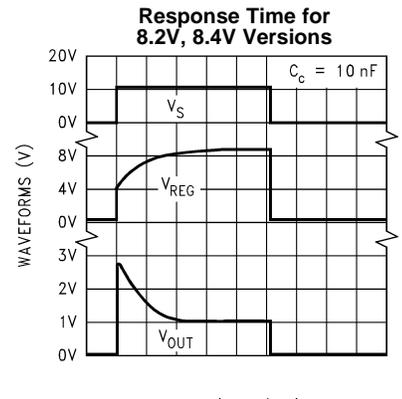


Figure 10.

TYPICAL PERFORMANCE CHARACTERISTICS (continued)

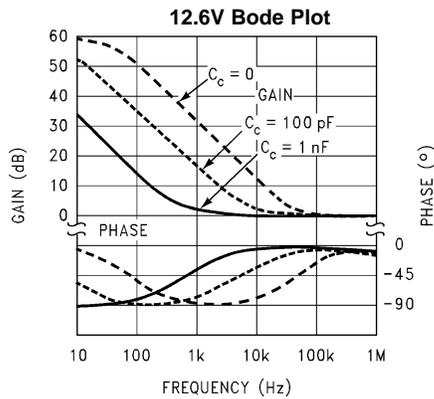


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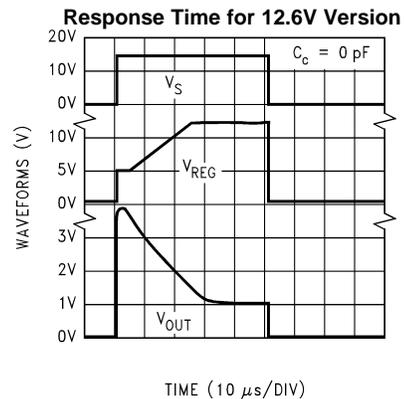


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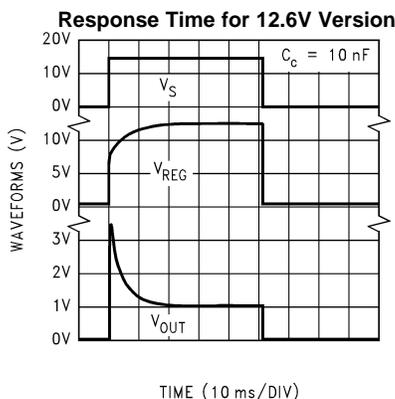


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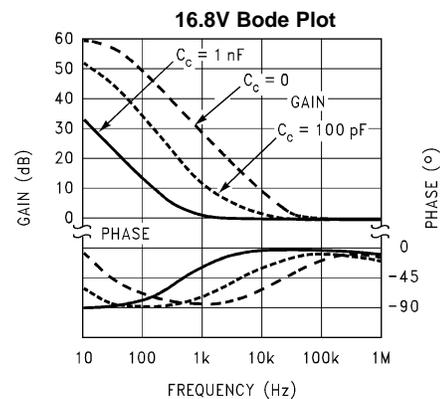


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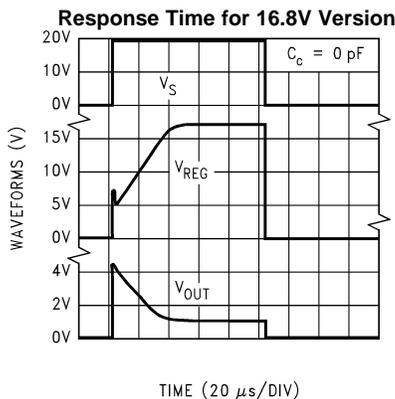


Figure 15.

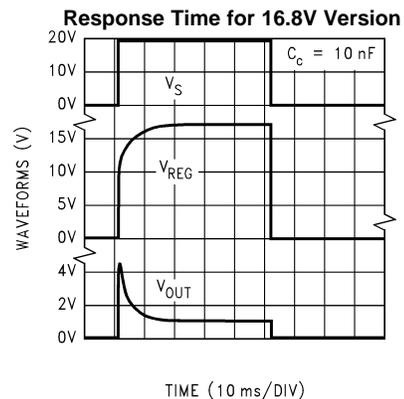


Figure 16.

TYPICAL PERFORMANCE CHARACTERISTICS (continued)

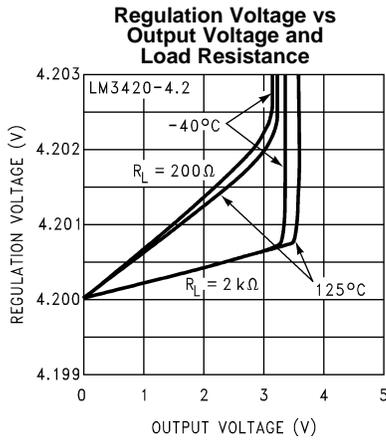


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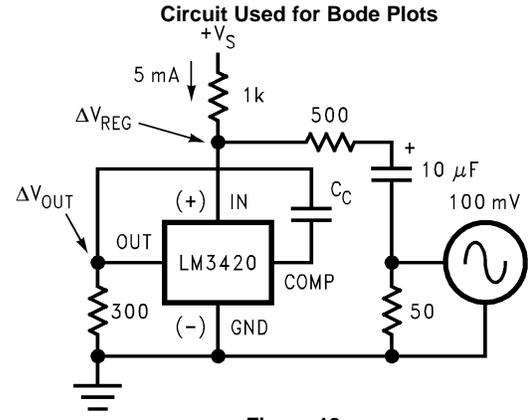


Figure 18.

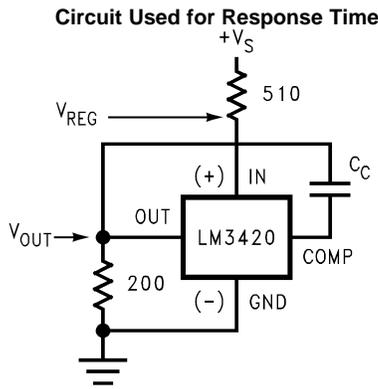


Figure 19.

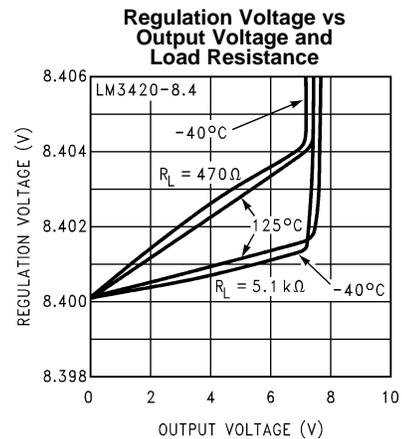


Figure 20.

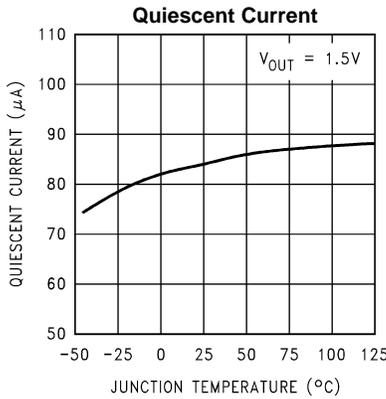


Figure 21.

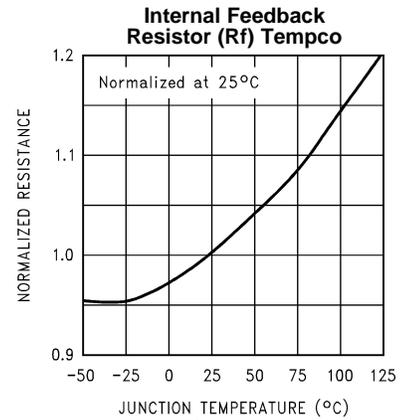


Figure 22.

TYPICAL PERFORMANCE CHARACTERISTICS (continued)

Regulation Voltage vs Output Voltage and Load Resistance

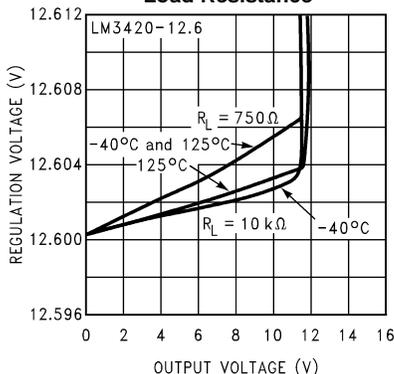


Figure 23.

Normalized Temperature Drift

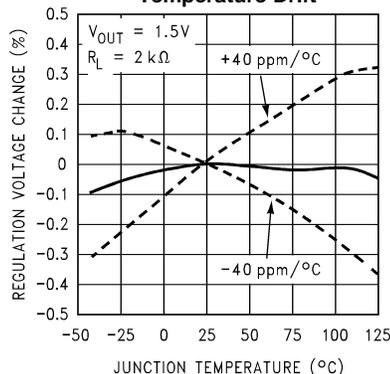


Figure 24.

Output Saturation Voltage (VSAT)

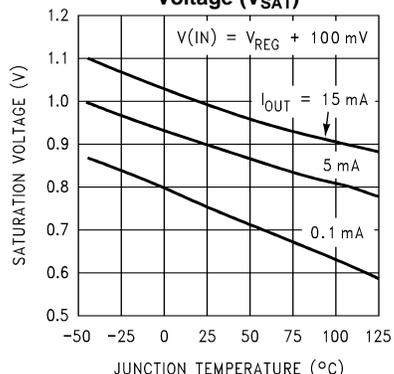


Figure 25.

Regulation Voltage vs Output Voltage and Load Resistance

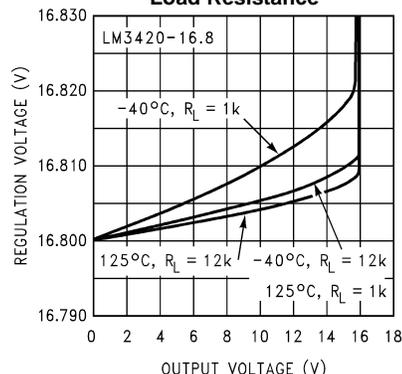


Figure 26.

PRODUCT DESCRIPTION

The LM3420 is a shunt regulator specifically designed to be the reference and control section in an overall feedback loop of a Lithium-Ion battery charger. The regulated output voltage is sensed between the IN pin and GROUND pin of the LM3420. If the voltage at the IN pin is less than the LM3420 regulating voltage (V_{REG}), the OUT pin sources no current. As the voltage at the IN pin approaches the V_{REG} voltage, the OUT pin begins sourcing current. This current is then used to drive a feedback device (opto-coupler), or a power device (linear regulator, switching regulator, etc.), which serves the output voltage to be the same value as V_{REG} .

In some applications, (even under normal operating conditions) the voltage on the IN pin can be forced above the V_{REG} voltage. In these instances, the maximum voltage applied to the IN pin should not exceed 20V. In addition, an external resistor may be required on the OUT pin to limit the maximum current to 20 mA.

Compensation

The inverting input of the error amplifier is brought out to allow overall closed-loop compensation. In many of the applications circuits shown here, compensation is provided by a single capacitor (C_C) connected from the compensation pin to the out pin of the LM3420. The capacitor values shown in the schematics are adequate under most conditions, but they can be increased or decreased depending on the desired loop response. Applying a load pulse to the output of a regulator circuit and observing the resultant output voltage response is an easy method of determining the stability of the control loop.

Analyzing more complex feedback loops requires additional information.

The formula for AC gain at a frequency (f) is as follows;

$$\text{Gain (f)} = 1 + \frac{Z_f(f)}{R_f}$$

$$\text{where } Z_f(f) = \frac{1}{j \cdot 2\pi \cdot f \cdot C_C}$$

where

- $R_f \approx 75 \text{ k}\Omega$ for the 4.2V part
- $R_f \approx 181 \text{ k}\Omega$ for the 8.4V part
- $R_f \approx 287 \text{ k}\Omega$ for the 12.6V part
- $R_f \approx 392 \text{ k}\Omega$ for the 16.8V part

(1)

The resistor (R_f) in the formula is an internal resistor located on the die. Since this resistor value will affect the phase margin, the worst case maximum and minimum values are important when analyzing closed loop stability. The minimum and maximum room temperature values of this resistor are specified in the Electrical Characteristics section of this data sheet, and a curve showing the temperature coefficient is shown in the curves section. Minimum values of R_f result in lower phase margins.

Test Circuit

The test circuit shown in [Figure 27](#) can be used to measure and verify various LM3420 parameters. Test conditions are set by forcing the appropriate voltage at the V_{OUT} Set test point and selecting the appropriate R_L or I_{OUT} as specified in the Electrical Characteristics section. Use a DVM at the “measure” test points to read the data.

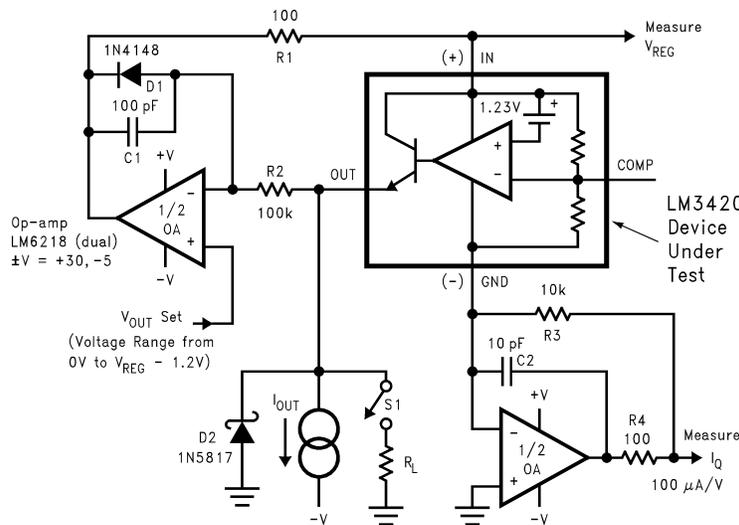


Figure 27. LM3420 Test Circuit

V_{REG} External Voltage Trim

The regulation voltage (V_{REG}) of the LM3420 can be externally trimmed by adding a single resistor from the COMP pin to the +IN pin or from the COMP pin to the GND pin, depending on the desired trim direction. Trim adjustments up to $\pm 10\%$ of V_{REG} can be realized, with only a small increase in the temperature coefficient. (See temperature coefficient curve shown in [Figure 28](#) below.)

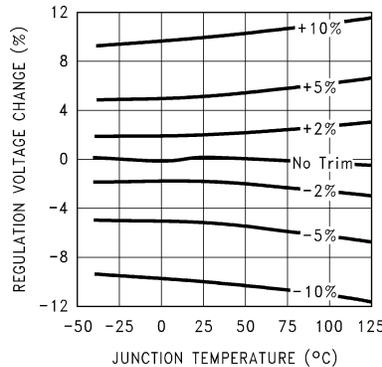


Figure 28. Normalized Temperature Drift with Output Externally Trimmed

Decreasing V_{REG}

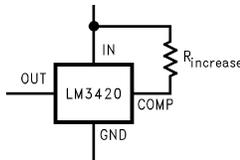


Figure 29. Increasing V_{REG}

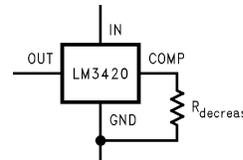


Figure 30. Changing V_{REG}

Formulas for selecting trim resistor values are shown below, based on the percent of increase (%incr) or percent of decrease (%decr) of the output voltage from the nominal voltage.

For LM3420-4.2

$$R_{\text{increase}} = 22 \times 10^5 / \% \text{incr} \tag{2}$$

$$R_{\text{decrease}} = (53 \times 10^5 / \% \text{decr}) - 75 \times 10^3 \tag{3}$$

For LM3420-8.2

$$R_{\text{increase}} = 26 \times 10^5 / \% \text{incr} \tag{4}$$

$$R_{\text{decrease}} = (150 \times 10^5 / \% \text{decr}) - 176 \times 10^3 \tag{5}$$

For LM3420-8.4

$$R_{\text{increase}} = 26 \times 10^5 / \% \text{incr} \tag{6}$$

$$R_{\text{decrease}} = (154 \times 10^5 / \% \text{decr}) - 181 \times 10^3 \tag{7}$$

For LM3420-12.6

$$R_{\text{increase}} = 28 \times 10^5 / \% \text{incr} \tag{8}$$

$$R_{\text{decrease}} = (259 \times 10^5 / \% \text{decr}) - 287 \times 10^3 \tag{9}$$

For LM3420-16.8

$$R_{\text{increase}} = 29 \times 10^5 / \% \text{incr} \tag{10}$$

$$R_{\text{decrease}} = (364 \times 10^5 / \% \text{decr}) - 392 \times 10^3 \tag{11}$$

APPLICATION INFORMATION

The LM3420 regulator/driver provides the reference and feedback drive functions for a Lithium-Ion battery charger. It can be used in many different charger configurations using both linear and switching topologies to provide the precision needed for charging Lithium-Ion batteries safely and efficiently. Output voltage tolerances better than 0.5% are possible without using trim pots or precision resistors. The circuits shown are designed for 2 cell operation, but they can readily be changed for either 1, 3 or 4 cell charging applications.

One item to keep in mind when designing with the LM3420 is that there are parasitic diodes present. In some designs, under special electrical conditions, unwanted currents may flow. Parasitic diodes exist from OUT to IN, as well as from GROUND to IN. In both instances the diode arrow is pointed toward the IN pin.

Application Circuits

The circuit shown in [Figure 31](#) performs constant-current, constant-voltage charging of two Li-Ion cells. At the beginning of the charge cycle, when the battery voltage is less than 8.4V, the LM3420 sources no current from the OUT pin, keeping Q2 off, thus allowing the LM317 Adjustable voltage regulator to operate as a constant-current source. (The LM317 is rated for currents up to 1.5A, and the LM350 and LM338 can be used for higher currents.) The LM317 forces a constant 1.25V across R_{LIM} , thus generating a constant current of

$$I_{LIM} = 1.25V/R_{LIM} \quad (12)$$

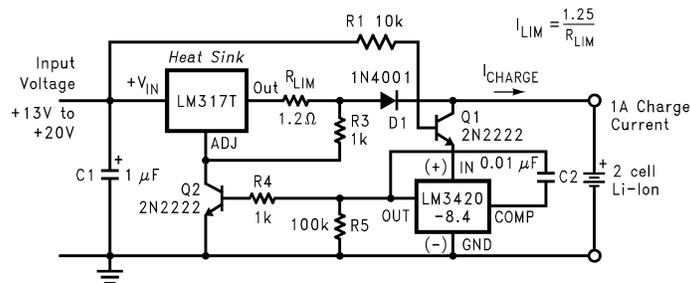


Figure 31. Constant Current/Constant Voltage Li-Ion Battery Charger

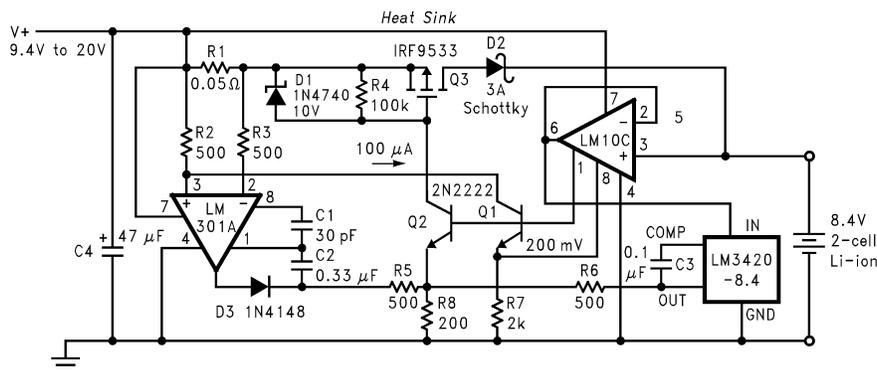


Figure 32. Low Drop-Out Constant Current/Constant Voltage 2-Cell Charger

Transistor Q1 provides a disconnect between the battery and the LM3420 when the input voltage is removed. This prevents the 85 µA quiescent current of the LM3420 from eventually discharging the battery. In this application Q1 is used as a low offset saturated switch, with the majority of the base drive current flowing through the collector and crossing over to the emitter as the battery becomes fully charged. It provides a very low collector to emitter saturation voltage (approximately 5 mV). Diode D1 is also used to prevent the battery current from flowing through the LM317 regulator from the output to the input when the DC input voltage is removed.

As the battery charges, its voltage begins to rise, and is sensed at the IN pin of the LM3420. Once the battery voltage reaches 8.4V, the LM3420 begins to regulate and starts sourcing current to the base of Q2. Transistor Q2 begins controlling the ADJ. pin of the LM317 which begins to regulate the voltage across the battery and the constant voltage portion of the charging cycle starts. Once the charger is in the constant voltage mode, the charger maintains a regulated 8.4V across the battery and the charging current is dependent on the state of charge of the battery. As the cells approach a fully charged condition, the charge current falls to a very low value.

Figure 32 shows a Li-Ion battery charger that features a dropout voltage of less than one volt. This charger is a constant-current, constant-voltage charger (it operates in constant-current mode at the beginning of the charge cycle and switches over to a constant-voltage mode near the end of the charging cycle). The circuit consists of two basic feedback loops. The first loop controls the constant charge current delivered to the battery, and the second determines the final voltage across the battery.

With a discharged battery connected to the charger, (battery voltage is less than 8.4V) the circuit begins the charge cycle with a constant charge current. The value of this current is set by using the reference section of the LM10C to force 200 mV across R7 thus causing approximately 100 μ A of emitter current to flow through Q1, and approximately 1 mA of emitter current to flow through Q2. The collector current of Q1 is also approximately 100 μ A, and this current flows through R2 developing 50 mV across it. This 50 mV is used as a reference to develop the constant charge current through the current sense resistor R1.

The constant current feedback loop operates as follows. Initially, the emitter and collector current of Q2 are both approximately 1 mA, thus providing gate drive to the MOSFET Q3, turning it on. The output of the LM301A op-amp is low. As Q3's current reaches 1A, the voltage across R1 approaches 50 mV, thus canceling the 50 mV drop across R2, and causing the op-amp's output to start going positive, and begin sourcing current into R8. As more current is forced into R8 from the op-amp, the collector current of Q2 is reduced by the same amount, which decreases the gate drive to Q3, to maintain a constant 50 mV across the 0.05 Ω current sensing resistor, thus maintaining a constant 1A of charge current.

The current limit loop is stabilized by compensating the LM301A with C1 (the standard frequency compensation used with this op-amp) and C2, which is additional compensation needed when D3 is forward biased. This helps speed up the response time during the reverse bias of D3. When the LM301A output is low, diode D3 reverse biases and prevents the op-amp from pulling more current through the emitter of Q2. This is important when the battery voltage reaches 8.4V, and the 1A charge current is no longer needed. Resistor R5 isolates the LM301A feedback node at the emitter of Q2.

The battery voltage is sensed and buffered by the op-amp section of the LM10C, connected as a voltage follower driving the LM3420. When the battery voltage reaches 8.4V, the LM3420 will begin regulating by sourcing current into R8, which controls the collector current of Q2, which in turn reduces the gate voltage of Q3 and becomes a constant voltage regulator for charging the battery. Resistor R6 isolates the LM3420 from the common feedback node at the emitter of Q2. If R5 and R6 are omitted, oscillations could occur during the transition from the constant-current to the constant-voltage mode. D2 and the PNP transistor input stage of the LM10C will disconnect the battery from the charger circuit when the input supply voltage is removed to prevent the battery from discharging.

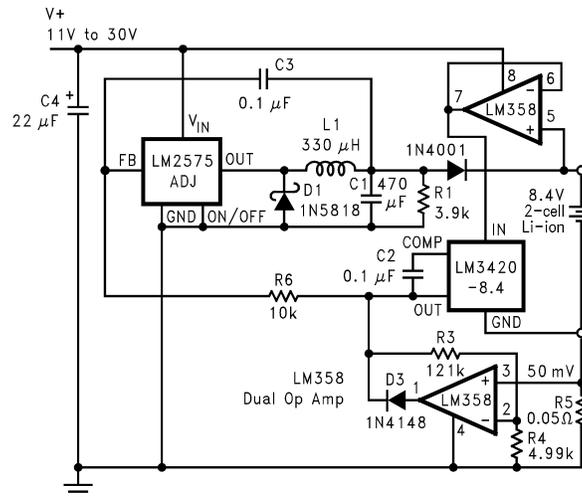


Figure 33. High Efficiency Switching Regulator Constant Current/Constant Voltage 2-Cell Charger

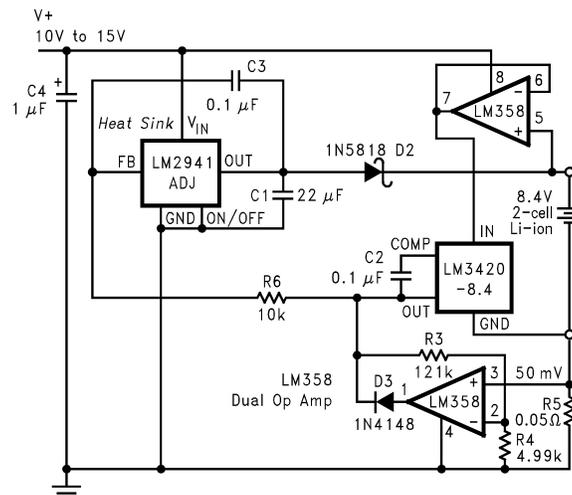


Figure 34. Low Dropout Constant Current/Constant Voltage Li-Ion Battery Charger

A switching regulator, constant-current, constant-voltage two-cell Li-Ion battery charging circuit is shown in [Figure 33](#). This circuit provides much better efficiency, especially over a wide input voltage range than the linear topologies. For a 1A charger an LM2575-ADJ. switching regulator IC is used in a standard buck topology. For other currents, or other packages, other members of the SIMPLE SWITCHER™ buck regulator family may be used.

Circuit operation is as follows. With a discharged battery connected to the charger, the circuit operates as a constant current source. The constant-current portion of the charger is formed by the loop consisting of one half of the LM358 op amp along with gain setting resistors R3 and R4, current sensing resistor R5, and the feedback reference voltage of 1.23V. Initially the LM358's output is low causing the output of the LM2575-ADJ. to rise thus causing some charging current to flow into the battery. When the current reaches 1A, it is sensed by resistor R5 (50 mΩ), and produces 50 mV. This 50 mV is amplified by the op-amps gain of 25 to produce 1.23V, which is applied to the feedback pin of the LM2575-ADJ. to satisfy the feedback loop.

Once the battery voltage reaches 8.4V, the LM3420 takes over and begins to control the feedback pin of the LM2575-ADJ. The LM3420 now regulates the voltage across the battery, and the charger becomes a constant-voltage charger. Loop compensation network R6 and C3 ensure stable operation of the charger circuit under both constant-current and constant-voltage conditions. If the input supply voltage is removed, diode D2 and the PNP input stage of the LM358 become reversed biased and disconnects the battery to ensure that the battery is not discharged. Diode D3 reverse biases to prevent the op-amp from sinking current when the charger changes to constant voltage mode.

The minimum supply voltage for this charger is approximately 11V, and the maximum is around 30V (limited by the 32V maximum operating voltage of the LM358). If another op-amp is substituted for the LM358, make sure that the input common-mode range of the op-amp extends down to ground so that it can accurately sense 50 mV. R1 is included to provide a minimum load for the switching regulator to assure that switch leakage current will not cause the output to rise when the battery is removed.

The circuit in Figure 34 is very similar to Figure 33, except the switching regulator has been replaced with a low dropout linear regulator, allowing the input voltage to be as low as 10V. The constant current and constant voltage control loops are the same as the previous circuit. Diode D2 has been changed to a Schottky diode to provide a reduction in the overall dropout voltage of this circuit, but Schottky diodes typically have higher leakage currents than a standard silicon diode. This leakage current could discharge the battery if the input voltage is removed for an extended period of time.

Another variation of a constant current/constant voltage switch mode charger is shown in Figure 35. The basic feedback loops for current and voltage are similar to the previous circuits. This circuit has the current sensing resistor, for the constant current part of the feedback loop, on the positive side of the battery, thus allowing a common ground between the input supply and the battery. Also, the LMC7101 op-amp is available in a very small SOT-23-5 package thus allowing a very compact pc board design. Diode D4 prevents the battery from discharging through the charger circuitry if the input voltage is removed, although the quiescent current of the LM3420 will still be present (approximately 85 μ A).

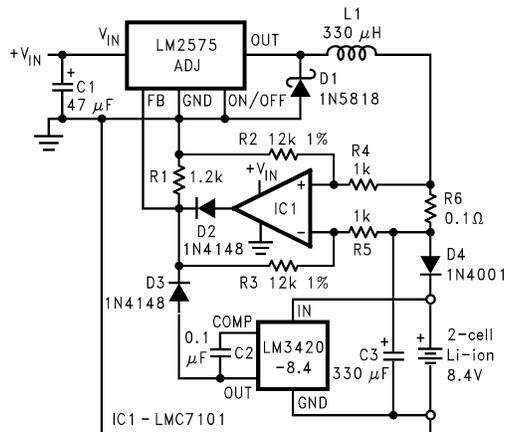


Figure 35. High Efficiency Switching Charger with High Side Current Sensing

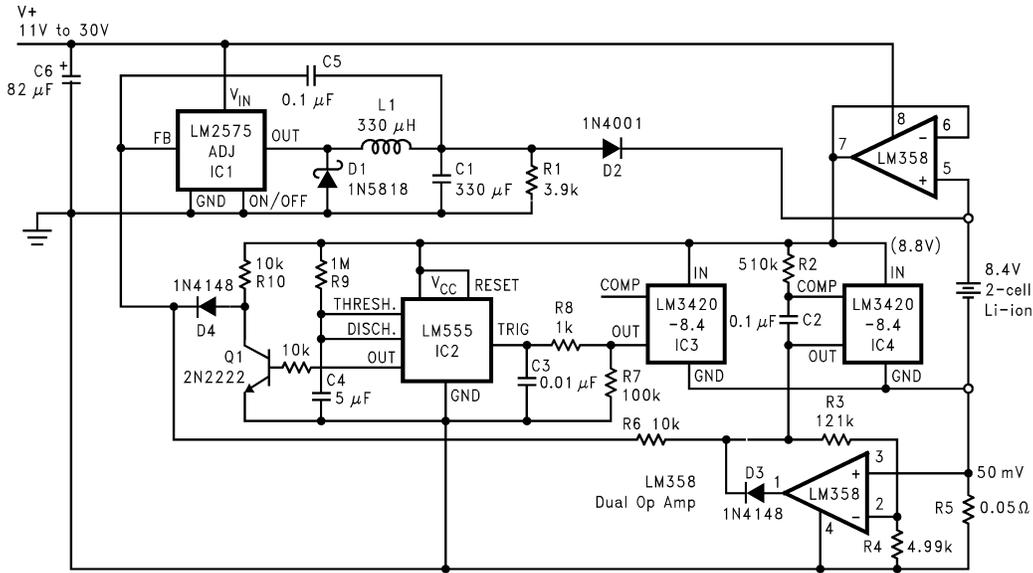


Figure 36. (Fast) Pulsed Constant Current 2-Cell Charger

A rapid charge Lithium-Ion battery charging circuit is shown in [Figure 36](#). This configuration uses a switching regulator to deliver the charging current in a series of constant current pulses. At the beginning of the charge cycle (constant-current mode), this circuit performs identically to the previous LM2575 charger by charging the battery at a constant current of 1A. As the battery voltage reaches 8.4V, this charger changes from a constant continuous current of 1A to a 5 second pulsed 1A. This allows the total battery charge time to be reduced considerably. This is different from the other charging circuits that switch from a constant current charge to a constant voltage charge once the battery voltage reaches 8.4V. After charging the battery with 1A for 5 seconds, the charge stops, and the battery voltage begins to drop. When it drops below 8.4V, the LM555 timer again starts the timing cycle and charges the battery with 1A for another 5 seconds. This cycling continues with a constant 5 second charge time, and a variable off time. In this manner, the battery will be charged with 1A for 5 seconds, followed by an off period (determined by the battery's state of charge), setting up a periodic 1A charge current. The off time is determined by how long it takes the battery voltage to decrease back down to 8.4V. When the battery first reaches 8.4V, the off time will be very short (1 ms or less), but when the battery approaches full charge, the off time will begin increasing to tens of seconds, then minutes, and eventually hours.

The constant-current loop for this charger and the method used for programming the 1A constant current is identical to the previous LM2575-ADJ. charger. In this circuit, a second LM3420-8.4 has its V_{REG} increased by approximately 400 mV (via R2), and is used to limit the output voltage of the charger to 8.8V in the event of a bad battery connection, or the battery is removed or possibly damaged.

The LM555 timer is connected as a one-shot, and is used to provide the 5 second charging pulses. As long as the battery voltage is less than the 8.4V, the output of IC3 will be held low, and the LM555 one-shot will never fire (the output of the LM555 will be held high) and the one-shot will have no effect on the charger. Once the battery voltage exceeds the 8.4V regulation voltage of IC3, the trigger pin of the LM555 is pulled high, enabling the one shot to begin timing. The charge current will now be pulsed into the battery at a 5 second rate, with the off time determined by the battery's state of charge. The LM555 output will go high for 5 seconds (pulling down the collector of Q1) which allows the 1A constant-current loop to control the circuit.

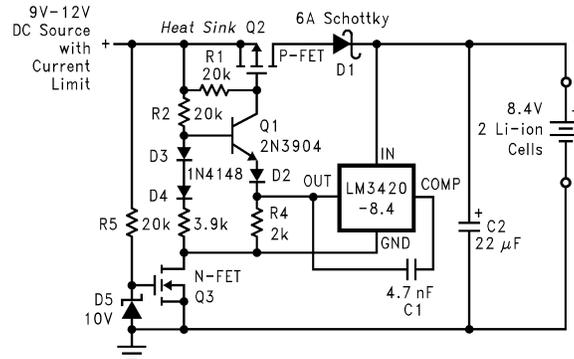


Figure 37. MOSFET Low Dropout Charger

Figure 37 shows a low dropout constant voltage charger using a MOSFET as the pass element, but this circuit does not include current limiting. This circuit uses Q3 and a Schottky diode to isolate the battery from the charging circuitry when the input voltage is removed, to prevent the battery from discharging. Q2 should be a high current (0.2Ω) FET, while Q3 can be a low current (2Ω) device.

Note: Although the application circuits shown here have been built and tested, they should be thoroughly evaluated with the same type of battery the charger will eventually be used with.

Different battery manufacturers may use a slightly different battery chemistry which may require different charging characteristics. Always consult the battery manufacturer for information on charging specifications and battery details, and always observe the manufacturers precautions when using their batteries. Avoid overcharging or shorting Lithium-Ion batteries.

REVISION HISTORY

Changes from Revision C (May 2013) to Revision D	Page
• Changed layout of National Data Sheet to TI format	19

PACKAGING INFORMATION

Orderable Device	Status (1)	Package Type	Package Drawing	Pins	Package Qty	Eco Plan (2)	Lead/Ball Finish	MSL Peak Temp (3)	Op Temp (°C)	Top-Side Markings (4)	Samples
LM3420AM5-8.4	ACTIVE	SOT-23	DBV	5	1000	TBD	Call TI	Call TI	-40 to 125	D03A	Samples
LM3420AM5-8.4/NOPB	ACTIVE	SOT-23	DBV	5	1000	Green (RoHS & no Sb/Br)	CU SN	Level-1-260C-UNLIM	-40 to 125	D03A	Samples
LM3420M5X-8.4	ACTIVE	SOT-23	DBV	5	3000	TBD	Call TI	Call TI	-40 to 125	D03B	Samples
LM3420M5X-8.4/NOPB	ACTIVE	SOT-23	DBV	5	3000	Green (RoHS & no Sb/Br)	CU SN	Level-1-260C-UNLIM	-40 to 125	D03B	Samples

(1) The marketing status values are defined as follows:

ACTIVE: Product device recommended for new designs.

LIFEBUY: TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

NRND: Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

PREVIEW: Device has been announced but is not in production. Samples may or may not be available.

OBSOLETE: TI has discontinued the production of the device.

(2) Eco Plan - The planned eco-friendly classification: Pb-Free (RoHS), Pb-Free (RoHS Exempt), or Green (RoHS & no Sb/Br) - please check <http://www.ti.com/productcontent> for the latest availability information and additional product content details.

TBD: The Pb-Free/Green conversion plan has not been defined.

Pb-Free (RoHS): TI's terms "Lead-Free" or "Pb-Free" mean semiconductor products that are compatible with the current RoHS requirements for all 6 substances, including the requirement that lead not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures, TI Pb-Free products are suitable for use in specified lead-free processes.

Pb-Free (RoHS Exempt): This component has a RoHS exemption for either 1) lead-based flip-chip solder bumps used between the die and package, or 2) lead-based die adhesive used between the die and leadframe. The component is otherwise considered Pb-Free (RoHS compatible) as defined above.

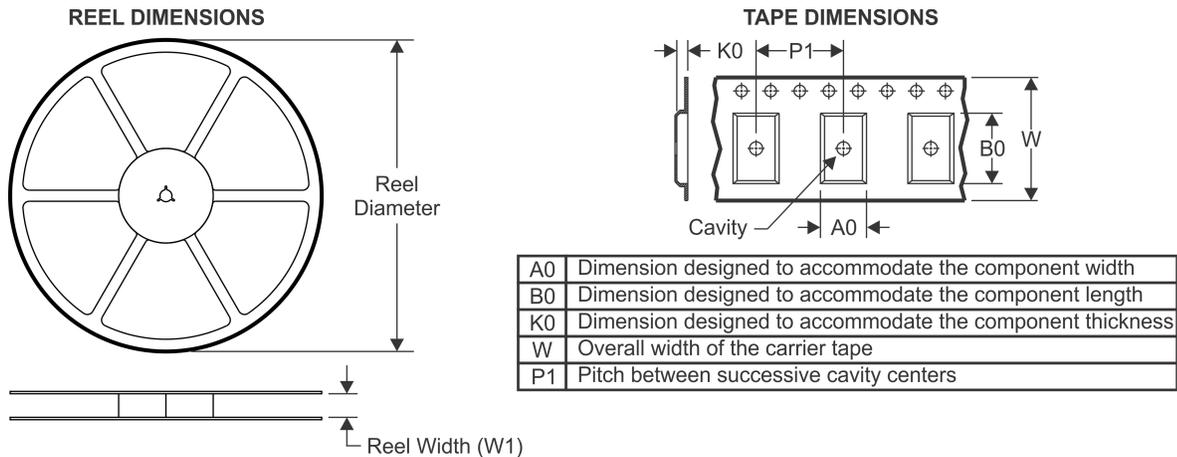
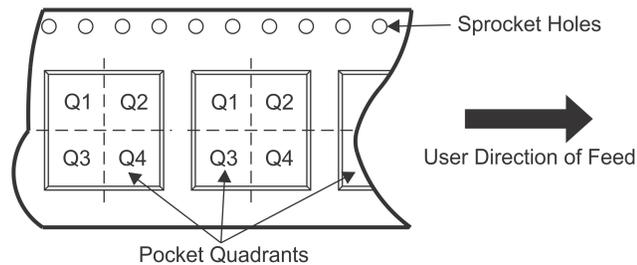
Green (RoHS & no Sb/Br): TI defines "Green" to mean Pb-Free (RoHS compatible), and free of Bromine (Br) and Antimony (Sb) based flame retardants (Br or Sb do not exceed 0.1% by weight in homogeneous material)

(3) MSL, Peak Temp. -- The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

(4) Multiple Top-Side Markings will be inside parentheses. Only one Top-Side Marking contained in parentheses and separated by a "~" will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Top-Side Marking for that device.

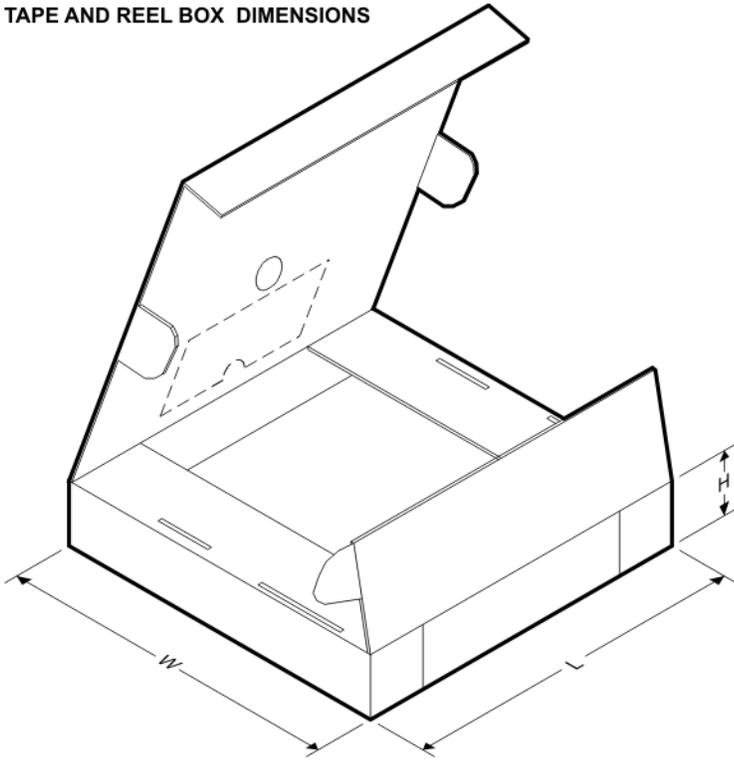
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TAPE AND REEL INFORMATION

QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE


*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Reel Diameter (mm)	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin1 Quadrant
LM3420AM5-8.4	SOT-23	DBV	5	1000	178.0	8.4	3.2	3.2	1.4	4.0	8.0	Q3
LM3420AM5-8.4/NOPB	SOT-23	DBV	5	1000	178.0	8.4	3.2	3.2	1.4	4.0	8.0	Q3
LM3420M5X-8.4	SOT-23	DBV	5	3000	178.0	8.4	3.2	3.2	1.4	4.0	8.0	Q3
LM3420M5X-8.4/NOPB	SOT-23	DBV	5	3000	178.0	8.4	3.2	3.2	1.4	4.0	8.0	Q3

TAPE AND REEL BOX DIMENSIONS


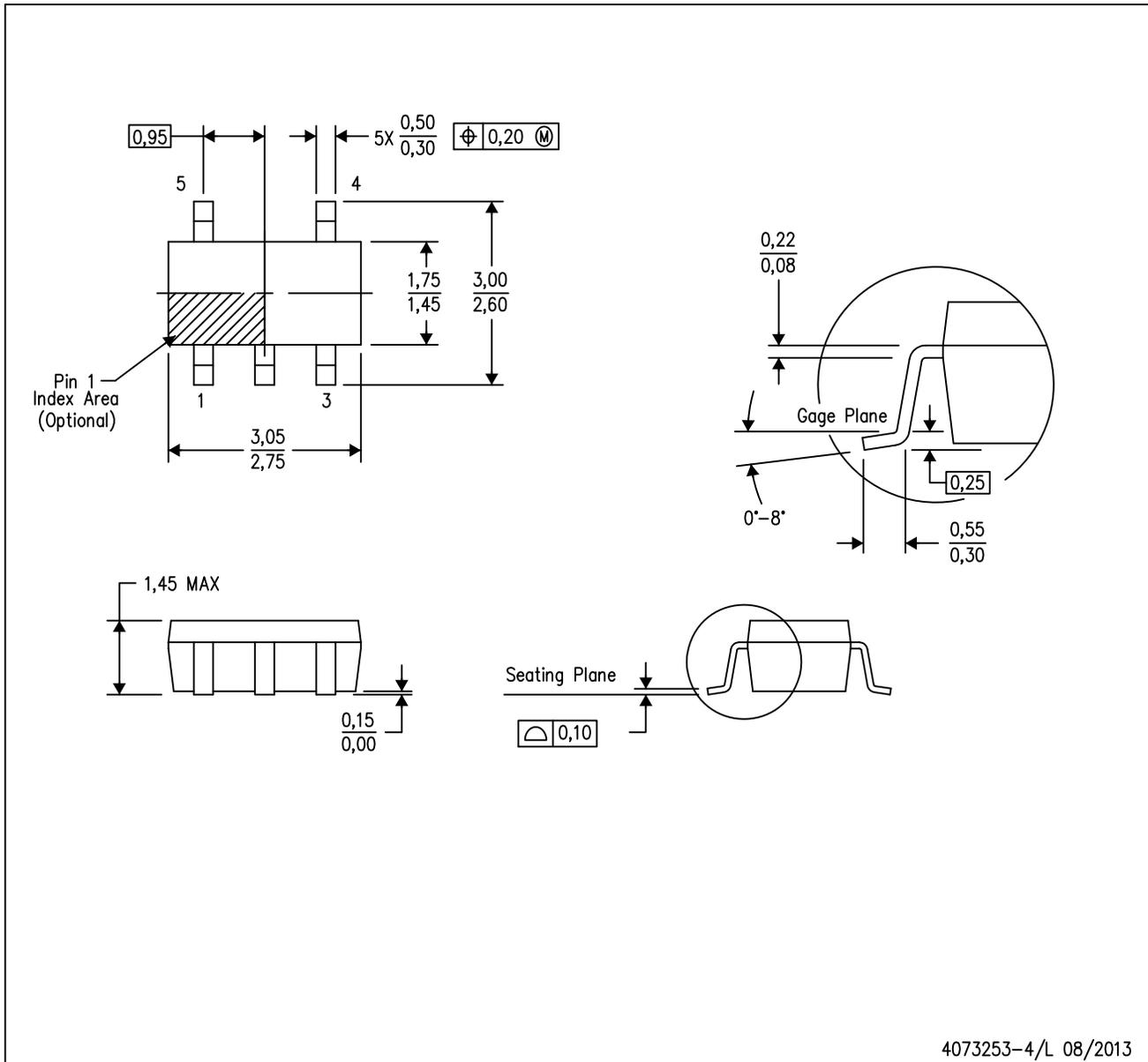
*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Length (mm)	Width (mm)	Height (mm)
LM3420AM5-8.4	SOT-23	DBV	5	1000	210.0	185.0	35.0
LM3420AM5-8.4/NOPB	SOT-23	DBV	5	1000	210.0	185.0	35.0
LM3420M5X-8.4	SOT-23	DBV	5	3000	210.0	185.0	35.0
LM3420M5X-8.4/NOPB	SOT-23	DBV	5	3000	210.0	185.0	35.0

MECHANICAL DATA

DBV (R-PDSO-G5)

PLASTIC SMALL-OUTLINE PACKAGE

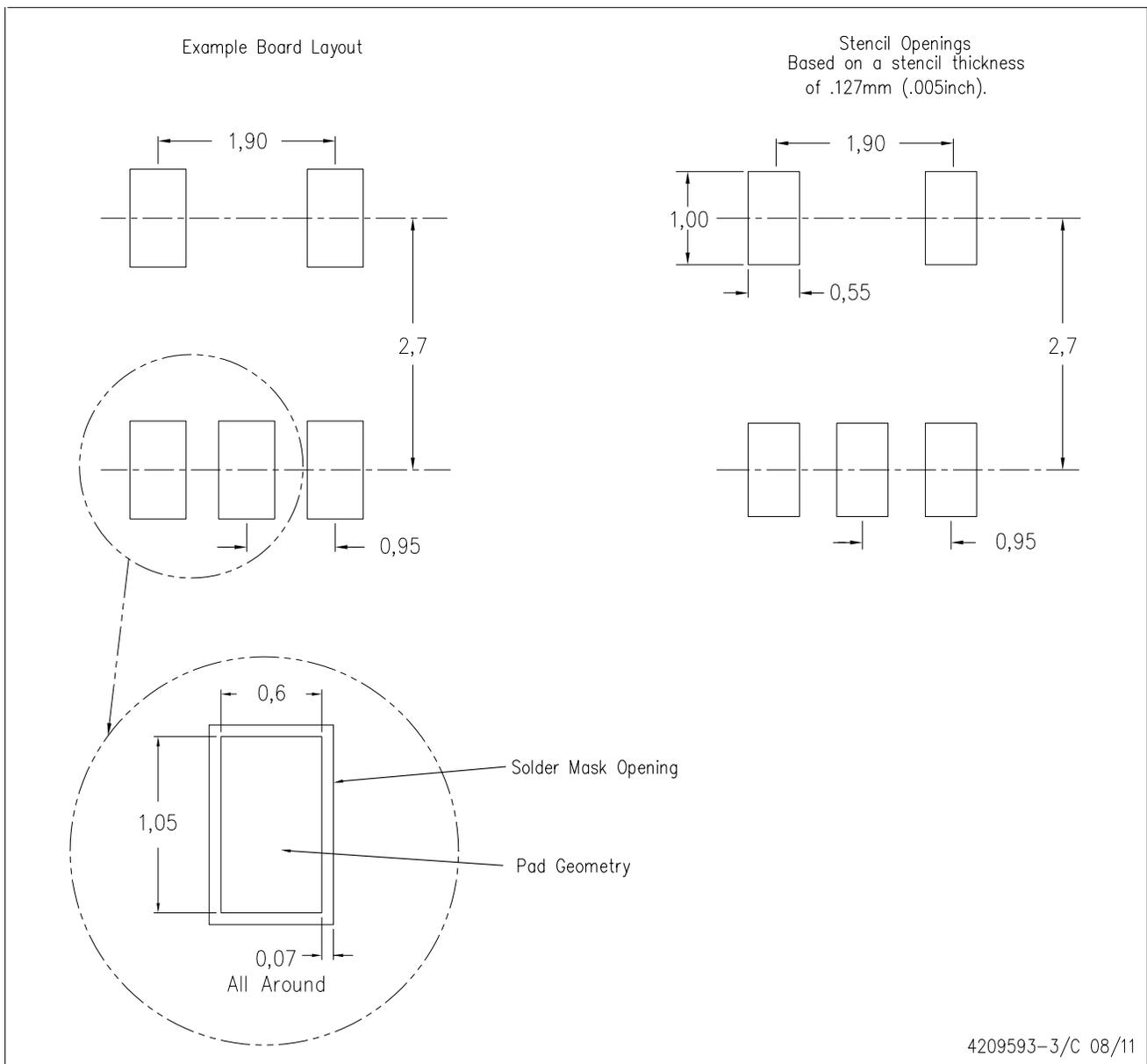


4073253-4/L 08/2013

- NOTES:
- A. All linear dimensions are in millimeters.
 - B. This drawing is subject to change without notice.
 - C. Body dimensions do not include mold flash or protrusion. Mold flash and protrusion shall not exceed 0.15 per side.
 - D. Falls within JEDEC MO-178 Variation AA.

DBV (R-PDSO-G5)

PLASTIC SMALL OUTLINE



- NOTES:
- A. All linear dimensions are in millimeters.
 - B. This drawing is subject to change without notice.
 - C. Customers should place a note on the circuit board fabrication drawing not to alter the center solder mask defined pad.
 - D. Publication IPC-7351 is recommended for alternate designs.
 - E. Laser cutting apertures with trapezoidal walls and also rounding corners will offer better paste release. Customers should contact their board assembly site for stencil design recommendations. Example stencil design based on a 50% volumetric metal load solder paste. Refer to IPC-7525 for other stencil recommendations.

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